

### FEATURES

- Low Noise, 80 nV p-p (0.1 Hz to 10 Hz)**  
3 nV/ $\sqrt{\text{Hz}}$  @ 1 kHz
- Low Drift, 0.2  $\mu\text{V}/^\circ\text{C}$**
- High Speed, 17 V/ $\mu\text{s}$  Slew Rate**  
63 MHz Gain Bandwidth
- Low Input Offset Voltage, 10  $\mu\text{V}$**
- Excellent CMRR, 126 dB (Common-Voltage @ 11 V)**
- High Open-Loop Gain, 1.8 Million**
- Replaces 725, OP-07, SE5534 In Gains > 5**
- Available in Die Form**

### GENERAL DESCRIPTION

The OP37 provides the same high performance as the OP27, but the design is optimized for circuits with gains greater than five. This design change increases slew rate to 17 V/ $\mu\text{s}$  and gain-bandwidth product to 63 MHz.

The OP37 provides the low offset and drift of the OP07 plus higher speed and lower noise. Offsets down to 25  $\mu\text{V}$  and a maximum drift of 0.6  $\mu\text{V}/^\circ\text{C}$  make the OP37 ideal for precision instrumentation applications. Exceptionally low noise ( $e_n = 3.5 \text{ nV/} @ 10 \text{ Hz}$ ), a low 1/f noise corner frequency of 2.7 Hz, and the high gain of 1.8 million, allow accurate high-gain amplification of low-level signals.

The low input bias current of 10 nA and offset current of 7 nA are achieved by using a bias-current cancellation circuit. Over the military temperature range this typically holds  $I_B$  and  $I_{OS}$  to 20 nA and 15 nA respectively.

The output stage has good load driving capability. A guaranteed swing of 10 V into 600  $\Omega$  and low output distortion make the OP37 an excellent choice for professional audio applications.

PSRR and CMRR exceed 120 dB. These characteristics, coupled with long-term drift of 0.2  $\mu\text{V}/\text{month}$ , allow the circuit designer to achieve performance levels previously attained only by discrete designs.

Low-cost, high-volume production of the OP37 is achieved by using on-chip zener-zap trimming. This reliable and stable offset trimming scheme has proved its effectiveness over many years of production history.

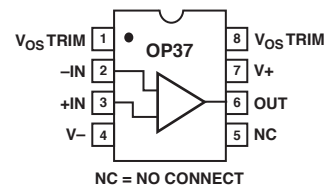
The OP37 brings low-noise instrumentation-type performance to such diverse applications as microphone, tapehead, and RIAA phono preamplifiers, high-speed signal conditioning for data acquisition systems, and wide-bandwidth instrumentation.

### PIN CONNECTIONS

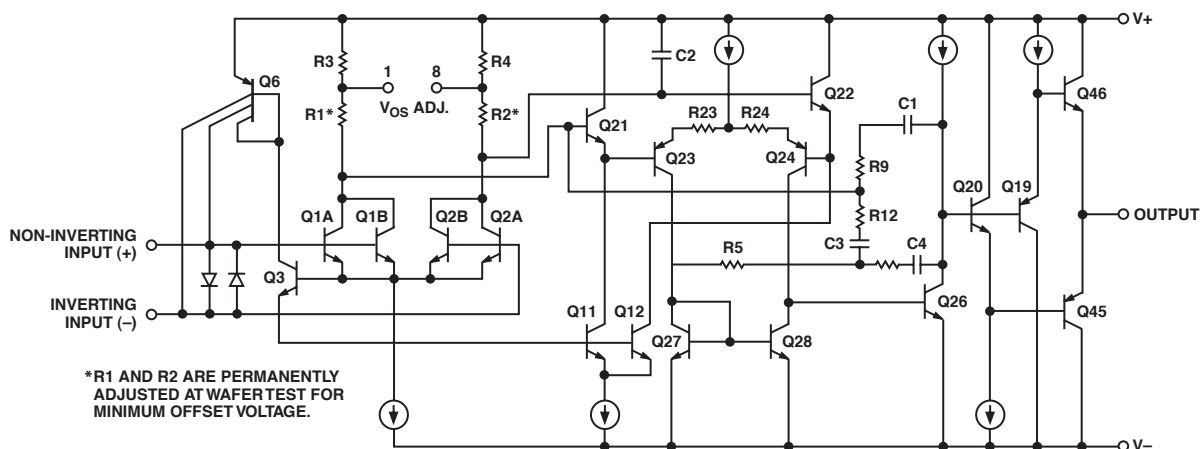
**8-Lead Hermetic DIP**  
(Z Suffix)

**Epoxy Mini-DIP**  
(P Suffix)

**8-Lead SO**  
(S Suffix)



### SIMPLIFIED SCHEMATIC



REV. B

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# OP37

## ABSOLUTE MAXIMUM RATINGS<sup>4</sup>

Supply Voltage	22 V
Internal Voltage (Note 1)	22 V
Output Short-Circuit Duration	Indefinite
Differential Input Voltage (Note 2)	0.7 V
Differential Input Current (Note 2)	25 mA
Storage Temperature Range	-65°C to +150°C
Operating Temperature Range	
OP37A	-55°C to +125°C
OP37E (Z)	-25°C to +85°C
OP37E, OP-37F (P)	0°C to 70°C
OP37G (P, S, Z)	-40°C to +85°C
Lead Temperature Range (Soldering, 60 sec)	300°C
Junction Temperature	-45°C to +150°C

Package Type	$\theta_{JA}^3$	$\theta_{JC}$	Unit
8-Lead Hermetic DIP (Z)	148	16	°C/W
8-Lead Plastic DIP (P)	103	43	°C/W
8-Lead SO (S)	158	43	°C/W

### NOTES

<sup>1</sup>For supply voltages less than 22 V, the absolute maximum input voltage is equal to the supply voltage.

<sup>2</sup>The OP37's inputs are protected by back-to-back diodes. Current limiting resistors are not used in order to achieve low noise. If differential input voltage exceeds 0.7 V, the input Current should be limited to 25 mA.

<sup>3</sup> $\theta_{JA}$  is specified for worst case mounting conditions, i.e.,  $\theta_{JA}$  is specified for device in socket for TO, CerDIP, P-DIP, and LCC packages;  $\theta_{JA}$  is specified for device soldered to printed circuit board for SO package.

<sup>4</sup>Absolute maximum ratings apply to both DICE and packaged parts, unless otherwise noted.

## ORDERING GUIDE

$T_A = 25^\circ\text{C}$ $V_{OS\ MAX}$ ( $\mu\text{V}$ )	CerDIP 8-Lead	Plastic 8-Lead	Operating Temperature Range
25	OP37AZ*		MIL
25	OP37EZ	OP37EP	IND/COM
60		OP37FP*	IND/COM
100		OP37GP	XIND
100	OP37GZ	OP37GS	XIND

\*Not for new design, obsolete, April 2002.

## CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the OP37 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high-energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.



# SPECIFICATIONS ( $V_S = \pm 15\text{ V}$ , $T_A = 25^\circ\text{C}$ , unless otherwise noted.)

Parameter	Symbol	Conditions	OP37A/E			OP37F			OP37G			Unit
			Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
Input Offset Voltage	$V_{OS}$	Note 1	10	25		20	60		30	100	$\mu\text{V}$	
Long-Term Stability	$V_{OS}/\text{Time}$	Notes 2, 3	0.2	1.0		0.3	1.5		0.4	2.0	$\mu\text{V}/\text{Mo}$	
Input Offset Current	$I_{OS}$		7	35		9	50		12	75	nA	
Input Bias Current	$I_B$		$\pm 10$	$\pm 40$		$\pm 12$	$\pm 55$		$\pm 15$	$\pm 80$	nA	
Input Noise Voltage	$e_{np-p}$	1 Hz to 10 Hz <sup>3, 5</sup>	0.08	0.18		0.08	0.18		0.09	0.25	$\mu\text{V p-p}$	
Input Noise Voltage Density	$e_n$	$f_0 = 10\text{ Hz}^3$ $f_0 = 30\text{ Hz}^3$ $f_0 = 1000\text{ Hz}^3$	3.5 3.1 3.0	5.5 4.5 3.8		3.5 3.1 3.0	5.5 4.5 3.8		3.8 3.3 3.2	8.0 5.6 4.5	$\text{nV}/\sqrt{\text{Hz}}$	
Input Noise Current Density	$i_N$	$f_0 = 10\text{ Hz}^3, 6$ $f_0 = 30\text{ Hz}^3, 6$ $f_0 = 1000\text{ Hz}^3, 6$	1.7 1.0 0.4	4.0 2.3 0.6		1.7 1.0 0.4	4.0 2.3 0.6		1.7 1.0 0.4	0.6	$\text{pA}/\sqrt{\text{Hz}}$	
Input Resistance Differential Mode	$R_{IN}$	Note 7	1.3	6		0.9	4.5		0.7	4	$\text{M}\Omega$	
Input Resistance Common Mode	$R_{INCM}$		3			2.5			2		$\text{G}\Omega$	
Input Voltage Range	IVR		$\pm 11$	$\pm 12.3$		$\pm 11$	$\pm 12.3$		$\pm 11$	$\pm 12.3$	V	
Common Mode Rejection Ratio	CMRR	$V_{CM} = \pm 11\text{ V}$	114	126		106	123		100	120	dB	
Power Supply Rejection Ratio	PSSR	$V_S = \pm 4\text{ V}$ to $\pm 18\text{ V}$	1	10		1	10		2	20	$\mu\text{V}/\text{V}$	
Large Signal Voltage Gain	$A_{VO}$	$R_L \geq 2\text{ k}\Omega$ , $V_O = \pm 10\text{ V}$ $R_L \geq 1\text{ k}\Omega$ , $V_O = \pm 10\text{ V}$ $R_L \geq 600\ \Omega$ , $V_O = \pm 1\text{ V}$ , $V_S \pm 4^4$	1000 800 250	1800 1500 700		1000 800 250	1800 1500 700		700 400 200	1500 1500 500	$\text{V}/\text{mV}$ $\text{V}/\text{mV}$ $\text{V}/\text{mV}$	
Output Voltage Swing	$V_O$	$R_L \geq 2\text{ k}\Omega$ $R_L \geq 600\ \Omega$ $R_L \geq 2\text{ k}\ \Omega^4$	$\pm 12.0$ $\pm 10$ 11	$\pm 13.8$ $\pm 11.5$ 17		$\pm 12.0$ $\pm 10$ 11	$\pm 13.8$ $\pm 11.5$ 17		$\pm 11.5$ $\pm 10$ 11	$\pm 13.5$ $\pm 11.5$ 17	V V $\text{V}/\mu\text{s}$	
Slew Rate	SR		11	17		11	17		11	17	$\text{V}/\mu\text{s}$	
Gain Bandwidth Product	GBW	$f_0 = 10\text{ kHz}^4$ $f_0 = 1\text{ MHz}$	45 40	63 40		45 40	63 40		45 40	63 40	MHz MHz	
Open-Loop Output Resistance	$R_O$	$V_O = 0, I_O = 0$	70			70			70		$\Omega$	
Power Consumption	$P_d$	$V_O = 0$	90	140		90	140		100	170	mW	
Offset Adjustment Range		$R_p = 10\text{ k}\Omega$	$\pm 4$			$\pm 4$			$\pm 4$		mV	

NOTES

- <sup>1</sup>Input offset voltage measurements are performed by automated test equipment approximately 0.5 seconds after application of power. A/E grades guaranteed fully warmed up.
- <sup>2</sup>Long term input offset voltage stability refers to the average trend line of  $V_{OS}$  vs. Time over extended periods after the first 30 days of operation. Excluding the initial hour of operation, changes in  $V_{OS}$  during the first 30 days are typically 2.5  $\mu\text{V}$ —refer to typical performance curve.
- <sup>3</sup>Sample tested.
- <sup>4</sup>Guaranteed by design.
- <sup>5</sup>See test circuit and frequency response curve for 0.1 Hz to 10 Hz tester.
- <sup>6</sup>See test circuit for current noise measurement.
- <sup>7</sup>Guaranteed by input bias current.

# OP37—SPECIFICATIONS

## Electrical Characteristics ( $V_S = \pm 15\text{ V}$ , $-55^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$ , unless otherwise noted.)

Parameter	Symbol	Conditions	OP37A			OP37C			Unit
			Min	Typ	Max	Min	Typ	Max	
Input Offset Voltage	$V_{OS}$	Note 1		10	25		30	100	$\mu\text{V}$
Average Input Offset Drift	$TCV_{OS}$ $TCV_{OSN}$	Note 2 Note 3		0.2	0.6		0.4	1.8	$\mu\text{V}/^\circ\text{C}$
Input Offset Current	$I_{OS}$			15	50		30	135	nA
Input Bias Current	$I_B$			$\pm 20$	$\pm 60$		$\pm 35$	$\pm 150$	nA
Input Voltage Range	IVR		$\pm 10.3$	$\pm 11.5$		$\pm 10.2$	$\pm 11.5$		V
Common Mode Rejection Ratio	CMRR	$V_{CM} = \pm 10\text{ V}$	108	122		94	116		dB
Power Supply Rejection Ratio	PSRR	$V_S = \pm 4.5\text{ V}$ to $\pm 18\text{ V}$		2	16		4	51	$\mu\text{V}/\text{V}$
Large-Signal Voltage Gain	$A_{VO}$	$R_L \geq 2\text{ k}\Omega$ , $V_O = \pm 10\text{ V}$	600	1200		300	800		V/mV
Output Voltage Swing	$V_O$	$R_L \geq 2\text{ k}\Omega$	$\pm 11.5$	$\pm 13.5$		$\pm 10.5$	$\pm 13.0$		V

## Electrical Characteristics ( $V_S = \pm 15\text{ V}$ , $-25^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$ for OP37EZ/FZ, $0^\circ\text{C} \leq T_A \leq 70^\circ\text{C}$ for OP37EP/FP, and $-40^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$ for OP37GP/GS/GZ, unless otherwise noted.)

Parameter	Symbol	Conditions	OP37E			OP37F			OP37C			Unit
			Min	Typ	Max	Min	Typ	Max	Min	Typ	Max	
Input Offset Voltage	$V_{OS}$			20	50		40	140		55	220	$\mu\text{V}$
Average Input Offset Drift	$TCV_{OS}$ $TCV_{OSN}$	Note 2 Note 3		0.2	0.6		0.3	1.3		0.4	1.8	$\mu\text{V}/^\circ\text{C}$
Input Offset Current	$I_{OS}$			10	50		14	85		20	135	nA
Input Bias Current	$I_B$			$\pm 14$	$\pm 60$		$\pm 18$	$\pm 95$		$\pm 25$	$\pm 150$	nA
Input Voltage Range	IVR		$\pm 10.5$	$\pm 11.8$		$\pm 10.5$	$\pm 11.8$		$\pm 10.5$	$\pm 11.8$		V
Common Mode Rejection Ratio	CMRR	$V_{CM} = \pm 10\text{ V}$	108	122		100	119		94	116		dB
Power Supply Rejection Ratio	PSRR	$V_S = \pm 4.5\text{ V}$ to $\pm 18\text{ V}$		2	15		2	16		4	32	$\mu\text{V}/\text{V}$
Large-Signal Voltage Gain	$A_{VO}$	$R_L \geq 2\text{ k}\Omega$ , $V_O = \pm 10\text{ V}$	750	1500		700	1300		450	1000		V/mV
Output Voltage Swing	$V_O$	$R_L \geq 2\text{ k}\Omega$	$\pm 11.7$	$\pm 13.6$		$\pm 11.4$	$\pm 13.5$		$\pm 11$	$\pm 13.3$		V

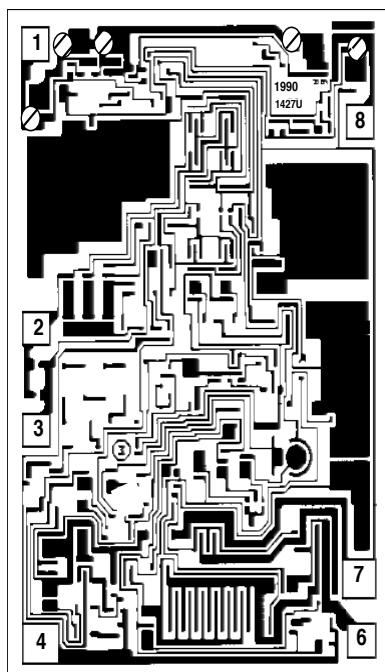
### NOTES

<sup>1</sup>Input offset voltage measurements are performed by automated test equipment approximately 0.5 seconds after application of power. A/E grades guaranteed fully warmed up.

<sup>2</sup>The  $TC_{VOS}$  performance is within the specifications unnullled or when nullled with  $R_p = 8\text{ k}\Omega$  to  $20\text{ k}\Omega$ .  $TC_{VOS}$  is 100% tested for A/E grades, sample tested for F/G grades.

<sup>3</sup>Guaranteed by design.

BINDING DIAGRAM



- 1. NULL
- 2. (-) INPUT
- 3. (+) INPUT
- 4. V-
- 6. OUTPUT
- 7. V+
- 8. NULL

**Wafer Test Limits** ( $V_S = \pm 15\text{ V}$ ,  $T_A = 25^\circ\text{C}$  for OP37N, OP37G, and OP37GR devices;  $T_A = 125^\circ\text{C}$  for OP37NT and OP37GT devices, unless otherwise noted.)

Parameter	Symbol	Conditions	OP37NT Limit	OP37N Limit	OP37GT Limit	OP37G Limit	OP37GR Limit	Unit
Input Offset Voltage	$V_{OS}$	Note 1	60	35	200	60	100	$\mu\text{V MAX}$
Input Offset Current	$I_{OS}$		50	35	85	50	75	nA MAX
Input Bias Current	$I_B$		$\pm 60$	$\pm 40$	$\pm 95$	$\pm 55$	$\pm 80$	nA MAX
Input Voltage Range	IVR		$\pm 10.3$	$\pm 11$	$\pm 10.3$	$\pm 11$	$\pm 11$	V MIN
Common Mode Rejection Ratio	CMRR	$V_{CM} = \pm 11\text{ V}$	108	114	100	106	100	dB MIN
Power Supply Rejection Ratio	PSRR	$T_A = 25^\circ\text{C}$ , $V_S = \pm 4\text{ V}$ to $\pm 18\text{ V}$	10	10	10	10	20	$\mu\text{V/V MAX}$
		$T_A = 125^\circ\text{C}$ , $V_S = \pm 4.5\text{ V}$ to $\pm 18\text{ V}$	16		20			$\mu\text{V/V MAX}$
Large-Signal Voltage Gain	$A_{VO}$	$R_L \geq 2\text{ k}\Omega$ , $V_O = \pm 10\text{ V}$	600	1000	500	1000	700	V/mV MIN
		$R_L \geq 1\text{ k}\Omega$ , $V_O = \pm 10\text{ V}$		800		800		V/mV MIN
Output Voltage Swing	$V_O$	$R_L \geq 2\text{ k}\Omega$ $R_L \geq 600\text{ k}\Omega$	$\pm 11.5$	$\pm 12$ $\pm 10$	$\pm 11$	$\pm 12$ $\pm 10$	$\pm 11.5$ $\pm 10$	V MIN V MIN
Power Consumption	$P_d$	$V_O = 0$		140		140	170	mW MAX

NOTES

For  $25^\circ\text{C}$  characteristics of OP37NT and OP37GT devices, see OP37N and OP37G characteristics, respectively.

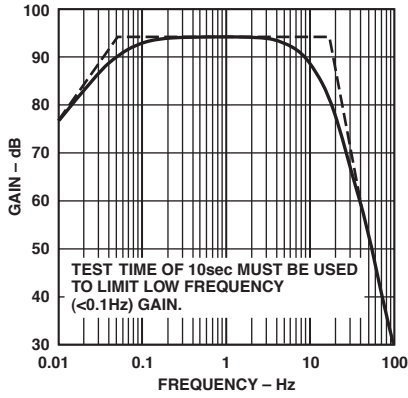
Electrical tests are performed at wafer probe to the limits shown. Due to variations in assembly methods and normal yield loss, yield after packaging is not guaranteed for standard product dice. Consult factory to negotiate specifications based on dice lot qualification through sample lot assembly and testing.

# OP37

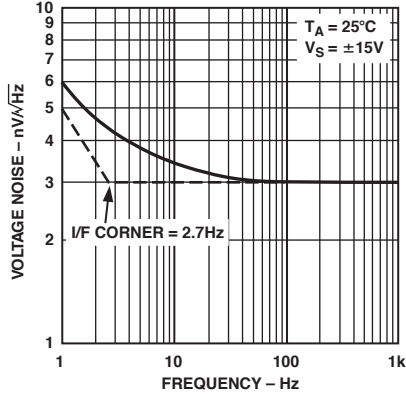
## Typical Electrical Characteristics ( $V_S = \pm 15\text{ V}$ , $T_A = 25^\circ\text{C}$ , unless otherwise noted.)

Parameter	Symbol	Conditions	OP37NT Typical	OP37N Typical	OP37GT Typical	OP37G Typical	OP37GR Typical	Unit
Average Input Offset Voltage Drift	$TCV_{OS}$ or $TCV_{OSN}$	Nulled or Unnulled $R_P = 8\text{ k}\Omega$ to $20\text{ k}\Omega$	0.2	0.2	0.3	0.3	0.4	$\mu\text{V}/^\circ\text{C}$
Average Input Offset Current Drift	$TCI_{OS}$		80	80	130	130	180	$\text{pA}/^\circ\text{C}$
Average Input Bias Current Drift	$TCI_B$		100	100	160	160	200	$\text{pA}/^\circ\text{C}$
Input Noise Voltage Density	$e_n$	$f_0 = 10\text{ Hz}$	3.5	3.5	3.5	3.5	3.8	$\text{nV}/\sqrt{\text{Hz}}$
		$f_0 = 30\text{ Hz}$	3.1	3.1	3.1	3.1	3.3	$\text{nV}/\sqrt{\text{Hz}}$
		$f_0 = 1000\text{ Hz}$	3.0	3.0	3.0	3.0	3.2	$\text{nV}/\sqrt{\text{Hz}}$
Input Noise Current Density	$i_n$	$f_0 = 10\text{ Hz}$	1.7	1.7	1.7	1.7	1.7	$\text{pA}/\sqrt{\text{Hz}}$
		$f_0 = 30\text{ Hz}$	1.0	1.0	1.0	1.0	1.0	$\text{pA}/\sqrt{\text{Hz}}$
		$f_0 = 1000\text{ Hz}$	0.4	0.4	0.4	0.4	0.4	$\text{pA}/\sqrt{\text{Hz}}$
Input Noise Voltage	$e_{n\text{ p-p}}$	0.1 Hz to 10 Hz	0.08	0.08	0.08	0.08	0.09	$\mu\text{V p-p}$
Slew Rate	SR	$R_L \geq 2\text{ k}\Omega$	17	17	17	17	17	$\text{V}/\mu\text{s}$
Gain Bandwidth Product	GBW	$f_0 = 10\text{ kHz}$	63	63	63	63	63	MHz

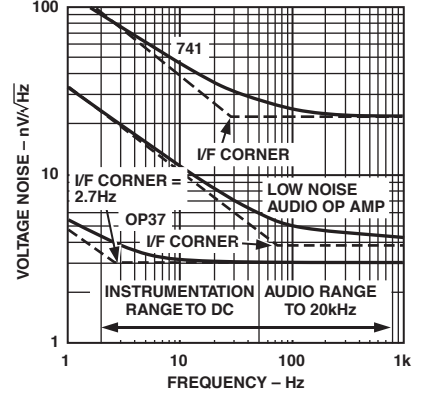
# Typical Performance Characteristics—OP37



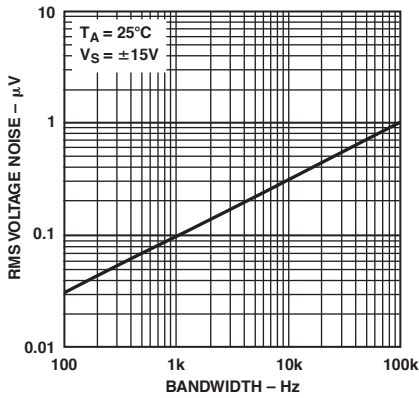
TPC 1. Noise-Tester Frequency Response (0.1 Hz to 10 Hz)



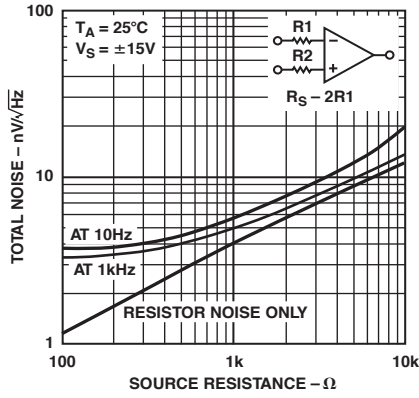
TPC 2. Voltage Noise Density vs. Frequency



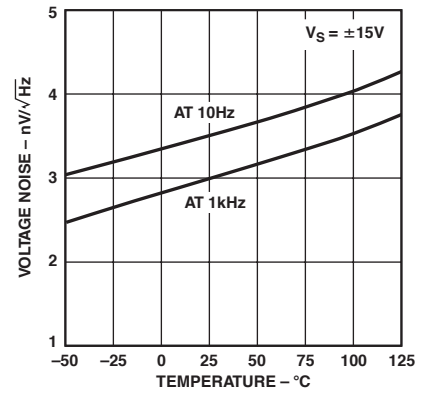
TPC 3. A Comparison of Op Amp Voltage Noise Spectra



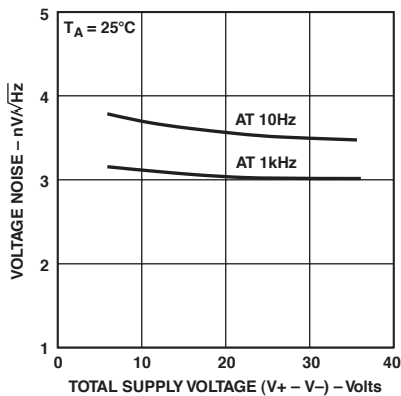
TPC 4. Input Wideband Voltage Noise vs. Bandwidth (0.1 Hz to Frequency Indicated)



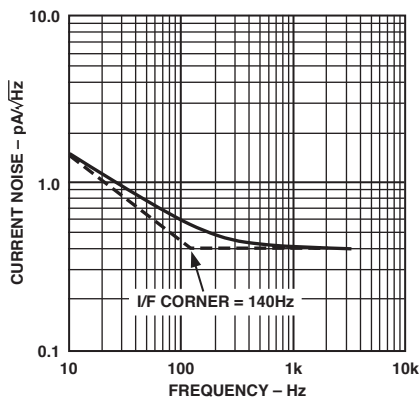
TPC 5. Total Noise vs. Source Resistance



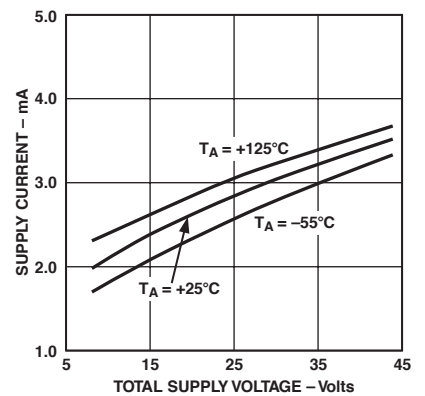
TPC 6. Voltage Noise Density vs. Temperature



TPC 7. Voltage Noise Density vs. Supply Voltage

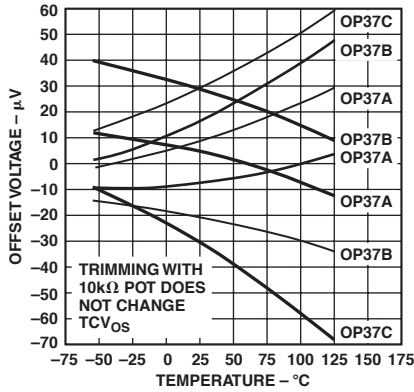


TPC 8. Current Noise Density vs. Frequency

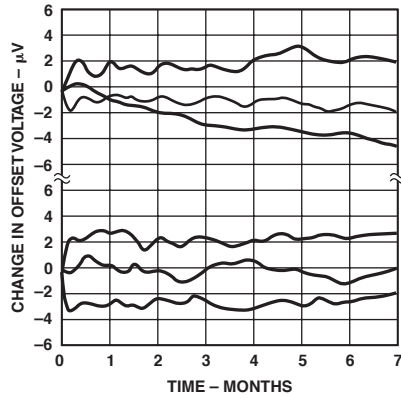


TPC 9. Supply Current vs. Supply Voltage

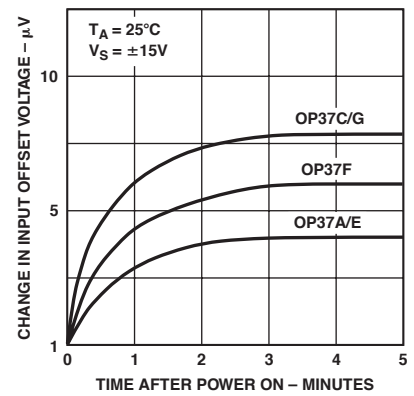
# OP37



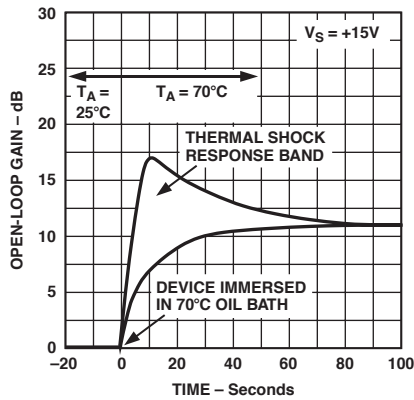
TPC 10. Offset Voltage Drift of Eight Representative Units vs. Temperature



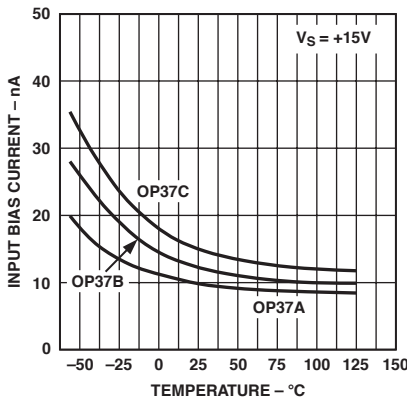
TPC 11. Long-Term Offset Voltage Drift of Six Representative Units



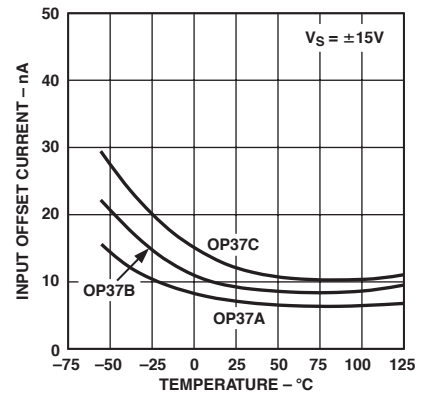
TPC 12. Warm Up Offset Voltage Drift



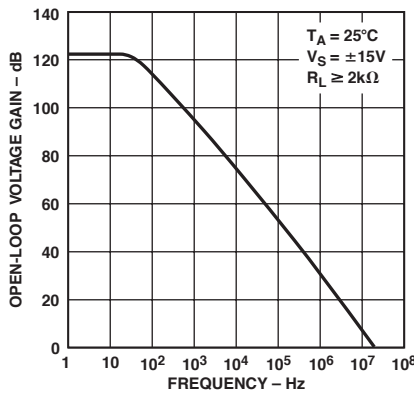
TPC 13. Offset Voltage Change Due to Thermal Shock



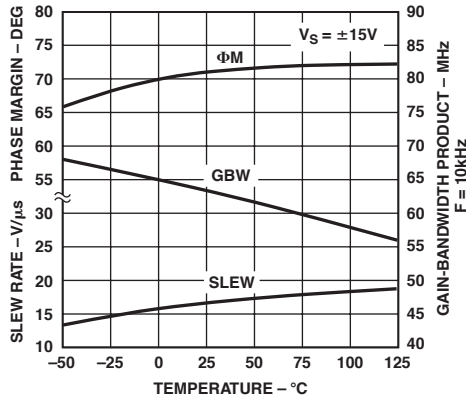
TPC 14. Input Bias Current vs. Temperature



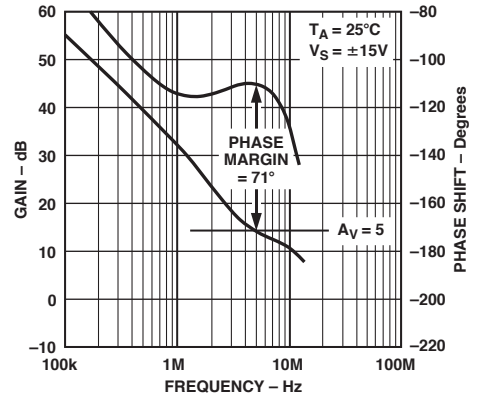
TPC 15. Input Offset Current vs. Temperature



TPC 16. Open-Loop Gain vs. Frequency

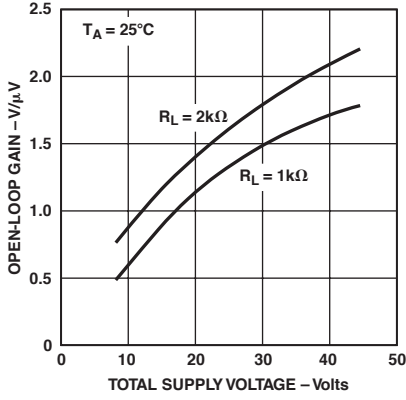


TPC 17. Slew Rate, Gain Bandwidth Product, Phase Margin vs. Temperature

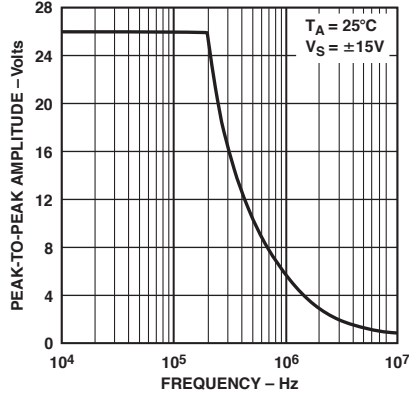


TPC 18. Gain, Phase Shift vs. Frequency

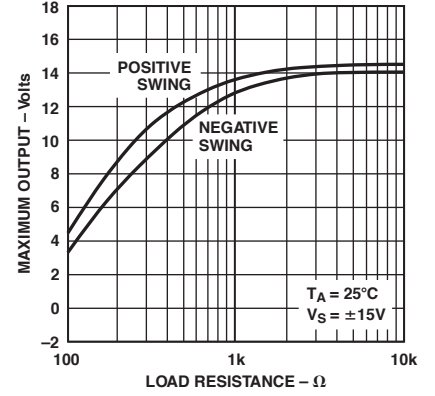




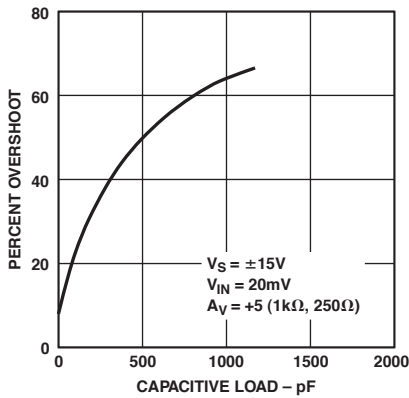
TPC 19. Open-Loop Voltage Gain vs. Supply Voltage



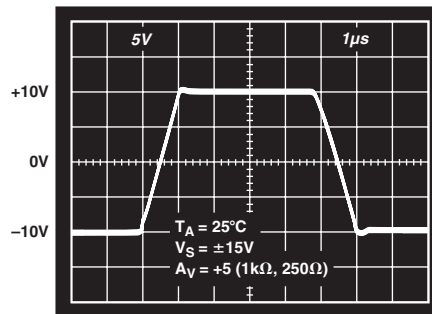
TPC 20. Maximum Output Swing vs. Frequency



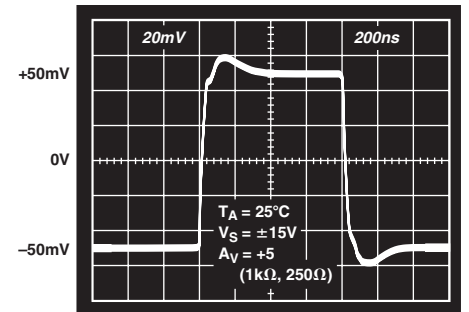
TPC 21. Maximum Output Voltage vs. Load Resistance



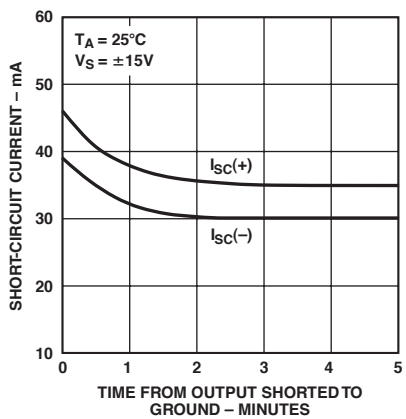
TPC 22. Small-Signal Overshoot vs. Capacitive Load



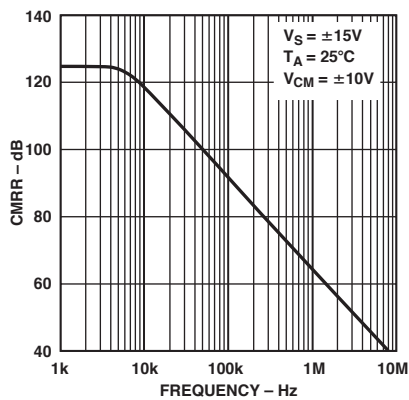
TPC 23. Large-Signal Transient Response



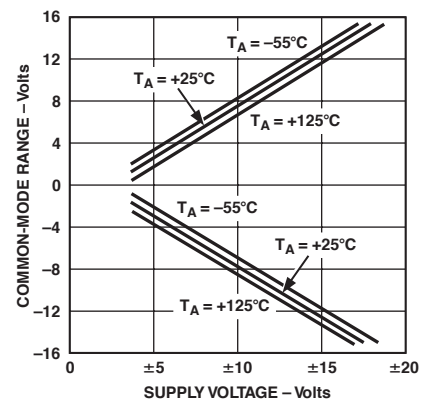
TPC 24. Small-Signal Transient Response



TPC 25. Short-Circuit Current vs. Time

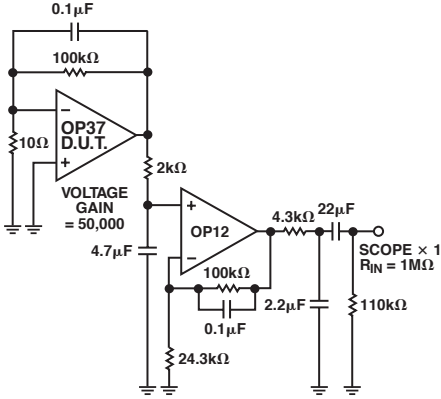


TPC 26. CMRR vs. Frequency

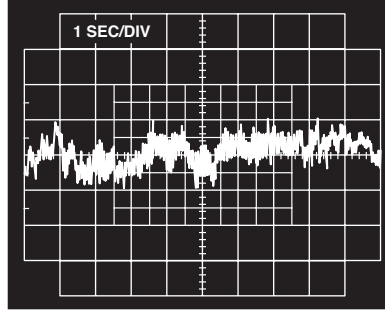


TPC 27. Common-Mode Input Range vs. Supply Voltage

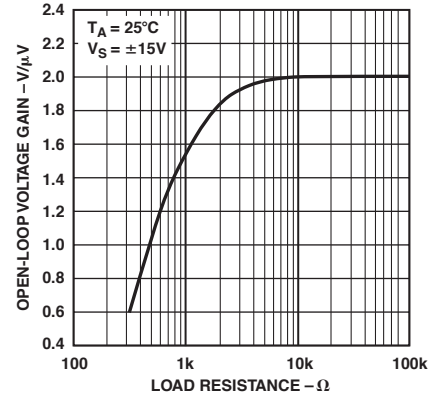
# OP37



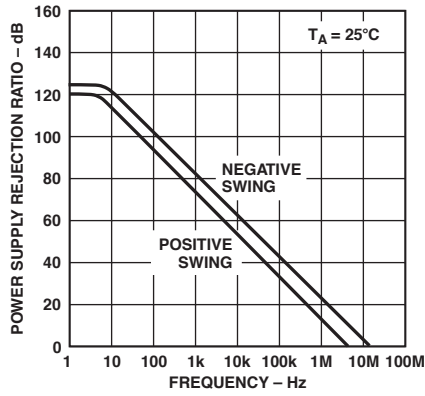
TPC 28. Noise Test Circuit (0.1 Hz to 10 Hz)



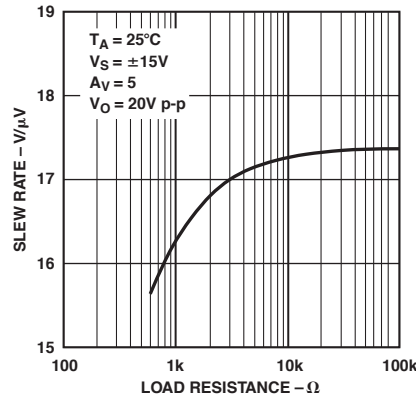
TPC 29. Low-Frequency Noise



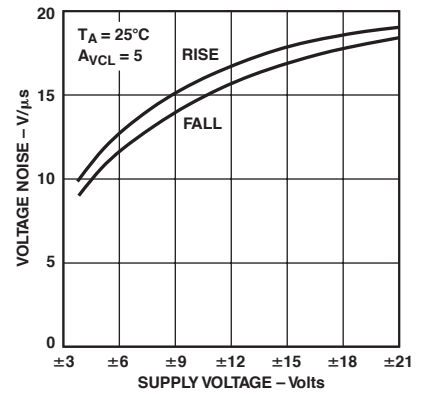
TPC 30. Open-Loop Voltage Gain vs. Load Resistance



TPC 31. PSRR vs. Frequency



TPC 32. Slew Rate vs. Load



TPC 33. Slew Rate vs. Supply Voltage



# OP37

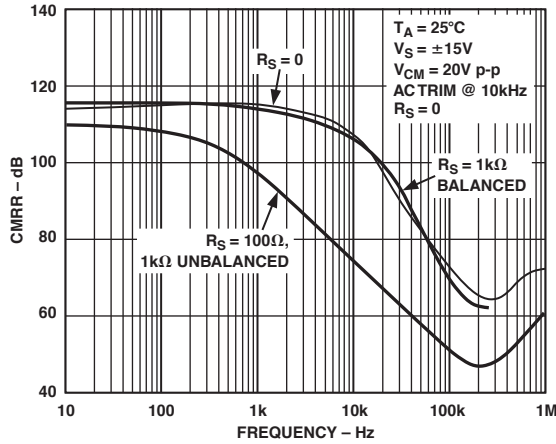


Figure 4b. CMRR vs. Frequency

### Comments on Noise

The OP37 is a very low-noise monolithic op amp. The outstanding input voltage noise characteristics of the OP37 are achieved mainly by operating the input stage at a high quiescent current. The input bias and offset currents, which would normally increase, are held to reasonable values by the input bias current cancellation circuit. The OP37A/E has  $I_B$  and  $I_{OS}$  of only  $\pm 40$  nA and 35 nA respectively at 25°C. This is particularly important when the input has a high source resistance. In addition, many audio amplifier designers prefer to use direct coupling. The high  $I_B$ ,  $TCV_{OS}$  of previous designs have made direct coupling difficult, if not impossible, to use.

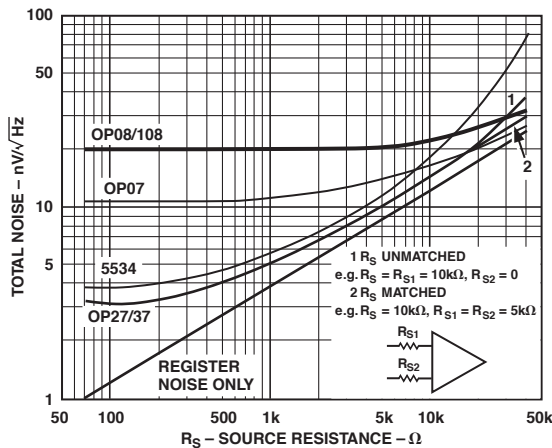


Figure 5. Noise vs. Resistance (Including Resistor Noise @ 1000 Hz)

Voltage noise is inversely proportional to the square-root of bias current, but current noise is proportional to the square-root of bias current. The OP37's noise advantage disappears when high source-resistors are used. Figures 5, 6, and 7 compare OP-37 observed total noise with the noise performance of other devices in different circuit applications.

$$\text{Total noise} = [(\text{Voltage noise})^2 + (\text{current noise} \times RS)^2 + (\text{resistor noise})^2]^{1/2}$$

Figure 5 shows noise versus source resistance at 1000 Hz. The same plot applies to wideband noise. To use this plot, just multiply the vertical scale by the square-root of the bandwidth.

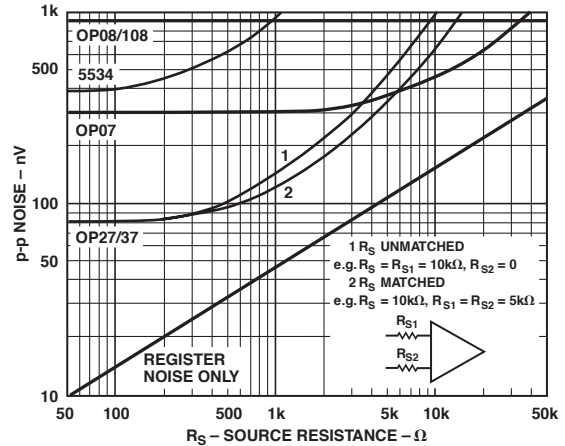


Figure 6. Peak-to-Peak Noise (0.1 Hz to 10 Hz) vs. Source Resistance (Includes Resistor Noise)

At  $R_S < 1$  k $\Omega$  key the OP37's low voltage noise is maintained. With  $R_S < 1$  k $\Omega$ , total noise increases, but is dominated by the resistor noise rather than current or voltage noise. It is only beyond  $R_S$  of 20 k $\Omega$  that current noise starts to dominate. The argument can be made that current noise is not important for applications with low to-moderate source resistances. The crossover between the OP37 and OP07 and OP08 noise occurs in the 15 k $\Omega$  to 40 k $\Omega$  region.

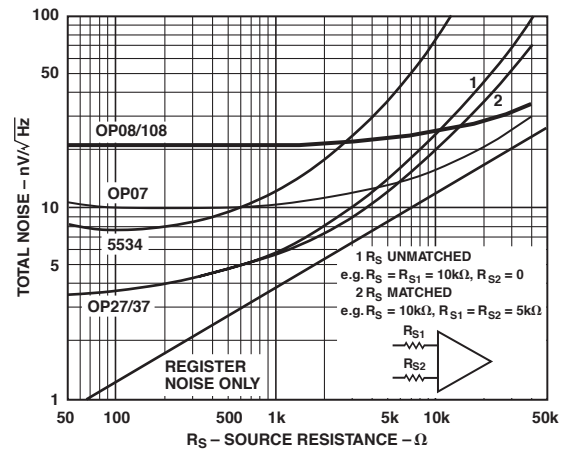


Figure 7. Noise vs. Source resistance (Includes Resistor Noise @ 10 Hz)

Figure 6 shows the 0.1 Hz to 10 Hz peak-to-peak noise. Here the picture is less favorable; resistor noise is negligible, current noise becomes important because it is inversely proportional to the square-root of frequency. The crossover with the OP07 occurs in the 3 k $\Omega$  to 5 k $\Omega$  range depending on whether balanced or unbalanced source resistors are used (at 3 k $\Omega$  the  $I_B$ ,  $I_{OS}$  error also can be three times the  $V_{OS}$  spec.).

Therefore, for low-frequency applications, the OP07 is better than the OP27/37 when  $R_S > 3$  k $\Omega$ . The only exception is when gain error is important. Figure 7 illustrates the 10 Hz noise. As expected, the results are between the previous two figures.

For reference, typical source resistances of some signal sources are listed in Table I.

Table I.

Device	Source Impedance	Comments
Strain Gauge	<500 Ω	Typically used in low-frequency applications.
Magnetic Tapehead	<1500 Ω	Low I <sub>B</sub> very important to reduce set-magnetization problems when direct coupling is used. OP37 I <sub>B</sub> can be neglected.
Magnetic Phonograph Cartridges	<1500 Ω	Similar need for low I <sub>B</sub> in direct coupled applications. OP37 will not introduce any self-magnetization problem.
Linear Variable Differential Transformer	<1500 Ω	Used in rugged servo-feedback applications. Bandwidth of interest is 400 Hz to 5 kHz.

**Audio Applications**

The following applications information has been abstracted from a PMI article in the 12/20/80 issue of Electronic Design magazine and updated.

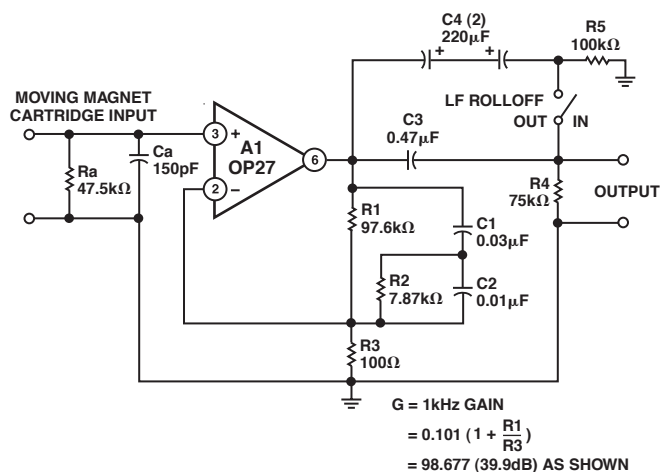


Figure 8. Phono Pre-Amplifier Circuit

Figure 8 is an example of a phono pre-amplifier circuit using the OP27 for A1; R1-R2-C1-C2 form a very accurate RIAA network with standard component values. The popular method to accomplish RIAA phono equalization is to employ frequency-dependent feedback around a high-quality gain block. Properly chosen, an RC network can provide the three necessary time constants of 3180 μs, 318 μs, and 75 μs.<sup>1</sup>

For initial equalization accuracy and stability, precision metal-film resistors and film capacitors of polystyrene or polypropylene are recommended since they have low voltage coefficients, dissipation factors, and dielectric absorption.<sup>4</sup> (High-K ceramic capacitors should be avoided here, though low-K ceramics—such as NPO types, which have excellent dissipation factors, and somewhat lower dielectric absorption—can be considered for small values or where space is at a premium.)

The OP37 brings a 3.2 nV/√Hz voltage noise and 0.45 pA/√Hz current noise to this circuit. To minimize noise from other sources, R3 is set to a value of 100 Ω, which generates a voltage noise of 1.3 nV/√Hz. The noise increases the 3.2 nV/√Hz of the amplifier

by only 0.7 dB. With a 1 kΩ source, the circuit noise measures 63 dB below a 1 mV reference level, unweighted, in a 20 kHz noise bandwidth.

Gain (G) of the circuit at 1 kHz can be calculated by the expression:

$$G = 0.101 \left( 1 + \frac{R_1}{R_3} \right)$$

For the values shown, the gain is just under 100 (or 40 dB). Lower gains can be accommodated by increasing R3, but gains higher than 40 dB will show more equalization errors because of the 8 MHz gain bandwidth of the OP27.

This circuit is capable of very low distortion over its entire range, generally below 0.01% at levels up to 7 V rms. At 3 V output levels, it will produce less than 0.03% total harmonic distortion at frequencies up to 20 kHz.

Capacitor C3 and resistor R4 form a simple -6 dB per octave rumble filter, with a corner at 22 Hz. As an option, the switch selected shunt capacitor C4, a nonpolarized electrolytic, bypasses the low-frequency rolloff. Placing the rumble filter's high-pass action after the preamp has the desirable result of discriminating against the RIAA amplified low frequency noise components and pickup-produced low-frequency disturbances.

A preamplifier for NAB tape playback is similar to an RIAA phono preamp, though more gain is typically demanded, along with equalization requiring a heavy low-frequency boost. The circuit in Figure 8 can be readily modified for tape use, as shown by Figure 9.

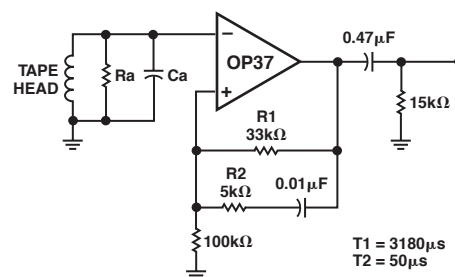


Figure 9. Tape-Head Preamplifier

While the tape-equalization requirement has a flat high frequency gain above 3 kHz (t<sub>2</sub> = 50 μs), the amplifier need not be stabilized for unity gain. The uncompensated OP37 provides a greater bandwidth and slew rate. For many applications, the idealized time constants shown may require trimming of Ra and R2 to optimize frequency response for non ideal tape head performance and other factors.<sup>5</sup>

The network values of the configuration yield a 50 dB gain at 1 kHz, and the dc gain is greater than 70 dB. Thus, the worst-case output offset is just over 500 mV. A single 0.47 μF output capacitor can block this level without affecting the dynamic range.

The tape head can be coupled directly to the amplifier input, since the worst-case bias current of 85 nA with a 400 mH, 100 μin. head (such as the PRB2H7K) will not be troublesome.

One potential tape-head problem is presented by amplifier bias-current transients which can magnetize a head. The OP27 and





